Rotary Actuators
Model Selection

Rotary Actuators Model Selection

(Refer to pages 338 to 343 for the selection of low-speed rotary actuators Series **CRQ2X/MSQX**.)

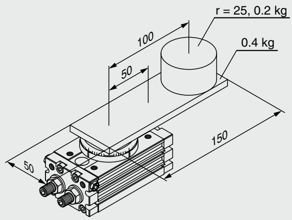
Selection Procedures | **Note** | **Selection Example**

◆ Operating conditions are as follows:

Operating conditions are as follows:
- Tentative models
- Operating pressure (MPa)
- Mounting orientation
- Load type
  - Static load
  - Resistance load
  - Inertial load
- Load dimensions (m)
- Load mass (kg)
- Rotation time (s)
- Rotation angle (rad)

Note:
- Refer to page 30 for the load type.
- The unit for the rotation angle is radian.
  180° = πrad
  90° = π/2rad

Selection Example:



Tentative model: MSQB30A Operating pressure: 0.3 MPa
Mounting orientation: Vertical Load type: Inertial load
Rotation time: t = 1.5s Rotation angle: θ = πrad (180°)

1 Calculation of Moment of Inertia

Calculate the inertial moment of load.
⇒P.24

Note:
- Loads are generated from multiple parts. The inertial moment of each load is calculated, and then totaled.

Selection Example:

Inertial moment of load 1 I_1

$$I_1 = 0.4 \times \frac{0.15^2 + 0.05^2}{12} + 0.4 \times 0.05^2 = 0.001833$$

Inertial moment of load 2 I_2

$$I_2 = 0.2 \times \frac{0.025^2}{2} + 0.2 \times 0.1^2 = 0.002063$$

Total inertial moment I

$$I = I_1 + I_2 = 0.003896 \text{ [kg·m}^2\text{]}$$

2 Calculation of Required Torque

Calculate the required torque for each load type and confirm whether the values fall in the effective torque range.
- Static load (Ts)
  Required torque: T = Ts
- Resistance load (Tf)
  Required torque: T = Tf (3 to 5)
- Inertial load (Ta)
  Required torque: T = Ta x 10

⇒P.30

Note:
- When the resistance load is rotated, the required torque calculated from the inertial load must be added.

  Required torque
  T = Tf x (3 to 5) + Ta x 10

Selection Example:

Inertial load: Ta

$$Ta = I \cdot \dot{\omega}$$

$$\dot{\omega} = \frac{2\theta}{t^2} \text{ [rad/s}^2\text{]}$$

Required torque: T

$$T = Ta \times 10$$

$$= 0.003896 \times \frac{2 \times \pi}{1.5^2} \times 10 = 0.109 \text{ [N·m]}$$

0.109 Nm < Effective torque OK

3 Confirmation of Rotation Time

Confirm whether the time falls in the rotation time adjustment range.
⇒P.33

Note:
- Consider the time after converted in the time per 90°.
  (1.0 s/180° is converted in 0.5 s/90°.)

Selection Example:

$0.2 \leq t \leq 1.0$
t = 0.75s/90°OK

4 Calculation of Kinetic Energy

Calculate the kinetic energy of the load and confirm whether the energy is below the allowable range.
Can confirm referring to the inertial moment and rotation time graph. (Pages 36 to 38)
⇒P.34

Note:
- If the energy exceeds the allowable range, a suitable cushioning mechanism such as a shock absorber must be externally installed.

Selection Example:

Kinetic energy: E

$$E = \frac{1}{2} I \cdot \omega^2$$

$$\omega = \frac{2 \cdot \theta}{t}$$

$$E = \frac{1}{2} 0.003896 \times \left(\frac{2 \times \pi}{1.5}\right)^2 = 0.03414 \text{ [J]}$$

0.03414 [J] < Allowable energy OK

5 Confirmation of Allowable Load

Confirm whether the load applied to the product is within the allowable range.
⇒P.39

Note:
- If the load exceeds the allowable range, a bearing or similar must be externally installed.

Selection Example:

Moment load: M

$$M = 0.4 \times 9.8 \times 0.05 + 0.2 \times 9.8 \times 0.1$$
$$= 0.392 \text{ [N·m]}$$

0.392 [N·m] < Allowable moment load OK

6 Calculation of Air Consumption and Required Air Flow Capacity

Air consumption and required air flow capacity are calculated when necessary. ⇒P.40

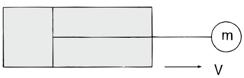
❶ Calculation of Moment of Inertia

The moment of inertia is a value indicating the inertia of a rotating body, and expresses the degree to which the body is difficult to rotate, or difficult to stop.
It is necessary to know the moment of inertia of the load in order to determine the value of necessary torque or kinetic energy when selecting a rotary actuator.

Moving the load with the actuator creates kinetic energy in the load. When stopping the moving load, it is necessary to absorb the kinetic energy of the load with a stopper or a shock absorber.
The kinetic energy of the load can be calculated using the formulas shown in Figure 1 (for linear motion) and Figure 2 (for rotation motion).

In the case of the kinetic energy for linear motion, the formula (1) shows that when the velocity v is constant, it is proportional to the mass m. In the case of rotation motion, the formula (2) shows that when the angular velocity is constant, it is proportional to the moment of inertia.

Linear motion

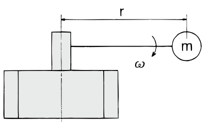


$$E = \frac{1}{2} \cdot m \cdot V^2 \quad \cdots\cdots\cdots\cdots\cdots (1)$$

E : Kinetic energy
m : Load mass
V : Speed

Fig. (1) Linear motion

Rotation motion



$$E = \frac{1}{2} \cdot I \cdot \omega^2 = \frac{1}{2} \cdot m \cdot r^2 \cdot \omega^2 \quad \cdots\cdots (2)$$

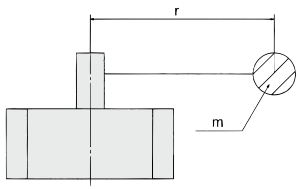
E : Kinetic energy
I : Moment of inertia (= $m \cdot r^2$)
ω : Speed
m : Mass
r : Radius of rotation

Fig. (2) Rotation motion

As the moment of inertia is proportional to the squares of the mass and the radius of rotation, even when the load mass is the same, the moment of inertia will be squared as the radius of rotation grows bigger. This will create greater kinetic energy, which may result in damage to the product.
When there is rotation motion, product selection should be based not on the load mass of the load, but on the moment of inertia.

Moment of Inertia Formula

The basic formula for obtaining a moment of inertia is shown below.



$$I = m \cdot r^2$$

m : Mass
r : Radius of rotation

This formula represents the moment of inertia for the shaft with mass m, which is located at distance r from the shaft.
For actual loads, the values of the moment of inertia are calculated depending on configurations, as shown on the following page.

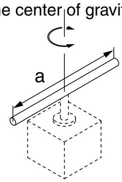
⇒P.25 Equation table of moment of inertia
⇒P.26 and 27 Calculation example of moment of inertia
⇒P.28 and 29 Graph for calculating the moment of inertia

❶-1 Equation Table of Moment of Inertia

I: Moment of inertia m: Load mass

1. Thin shaft

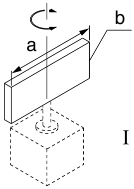
Position of rotational axis: Perpendicular to the shaft through the center of gravity



$$I = m \cdot \frac{a^2}{12}$$

2. Thin rectangular plate

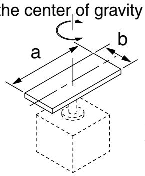
Position of rotational axis: Parallel to side b and through the center of gravity



$$I = m \cdot \frac{a^2}{12}$$

3. Thin rectangular plate (Including Rectangular parallelepiped)

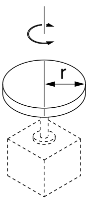
Position of rotational axis: Perpendicular to the plate through the center of gravity



$$I = m \cdot \frac{a^2 + b^2}{12}$$

4. Round plate (Including column)

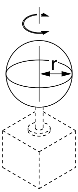
Position of rotational axis: Through the center axis



$$I = m \cdot \frac{r^2}{2}$$

5. Solid sphere

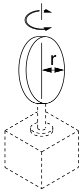
Position of rotational axis: Through the center of diameter



$$I = m \cdot \frac{2r^2}{5}$$

6. Thin round plate

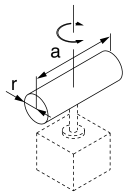
Position of rotational axis: Through the center of diameter



$$I = m \cdot \frac{r^2}{4}$$

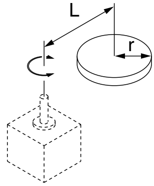
7. Cylinder

Position of rotational axis: Through the center of diameter and gravity.



$$I = m \cdot \frac{3r^2 + a^2}{12}$$

8. When the rotational axis and load center of gravity are not consistent

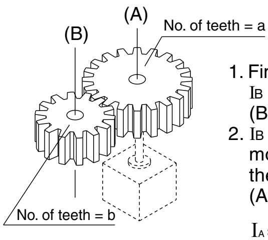


$$I = K + m \cdot L^2$$

K: Moment of inertia around the load center of gravity

4. Round plate $K = m \cdot \frac{r^2}{2}$

4. Gear transmission



1. Find the moment of inertia I_B for the rotation of shaft (B).
2. I_B is converted to the moment of inertia I_A for the rotation of the shaft (A).

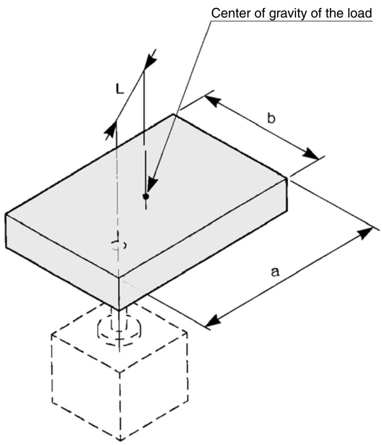
$$I_A = \left(\frac{a}{b}\right)^2 \cdot I_B$$

CRB2 -Z
CRBU2
CRB1
MSU
CRJ
CRA1 -Z
CRA1
CRQ2
MSQ
MSZ
CRQ2X MSQX
MRQ
D-□

Rotary Actuators Model Selection

❶-2 Calculation Example of Moment of Inertia

1 If the shaft is located at a desired point of the load:



Example: ① If the load is the thin rectangular plate:
Obtain the center of gravity of the load as I_1, a provisional shaft.

$$I_1 = m \cdot \frac{a^2 + b^2}{12}$$

② Obtain the actual moment of inertia I_2 around the shaft, with the premise that the mass of the load itself is concentrated in the load's center of gravity point.

$$I_2 = m \cdot L^2$$

③ Obtain the actual moment of inertia I.

$$I = I_1 + I_2$$

(m: mass of the load
L : distance from the shaft to the load's center of gravity)

Calculation Example

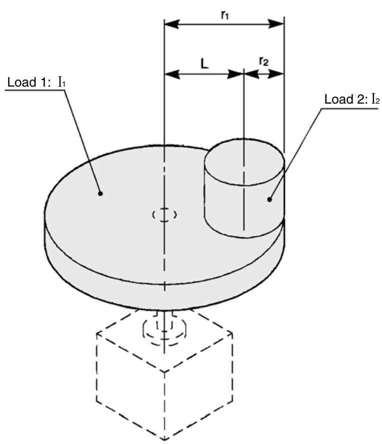
a = 0.2 m, b = 0.1 m, L = 0.05 m, m = 1.5 kg

$I_1 = 1.5 \times \frac{0.2^2 + 0.1^2}{12} = 6.25 \times 10^{-3}$ kg·m²

$I_2 = 1.5 \times 0.05^2 = 3.75 \times 10^{-3}$ kg·m²

$I = (6.25 + 3.75) \times 10^{-3} = 0.01$ kg·m²

2 If the load is divided into multiple loads:



Example: ① If the load is divided into the 2 cylinders:
{The center of gravity of load 1 matches the shaft
The center of gravity of load 2 differs from the shaft}
Obtain the moment of inertia of load 1:

$$I_1 = m_1 \cdot \frac{r_1^2}{2}$$

② Obtain the moment of inertia of load 2:

$$I_2 = m_2 \cdot \frac{r_2^2}{2} + m_2 \cdot L^2$$

③ Obtain the actual moment of inertia I:

$$I = I_1 + I_2$$

(m_1, m_2: mass of loads 1, and 2
r_1, r_2: radius of loads 1, and 2
L: distance from the shaft to the center of gravity of load 2)

Calculation Example

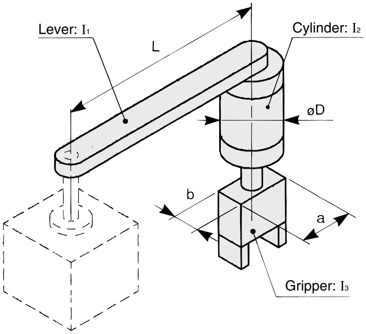
m_1 = 2.5 kg, m_2 = 0.5 kg, r_1 = 0.1 m, r_2 = 0.02 m, L = 0.08 m

$I_1 = 2.5 \times \frac{0.1^2}{2} = 1.25 \times 10^{-2}$ kg·m²

$I_2 = 0.5 \times \frac{0.02^2}{2} + 0.5 \times 0.08^2 = 0.33 \times 10^{-2}$ kg·m²

$I = (1.25 + 0.33) \times 10^{-2} = 1.58 \times 10^{-2}$ kg·m²

3 If a lever is attached to the shaft and a cylinder and a gripper are mounted to the tip of the lever:



Example: ① Obtain the lever's moment of inertia:

$$I_1 = m_1 \cdot \frac{L^2}{3}$$

② Obtain the cylinder's moment of inertia:

$$I_2 = m_2 \cdot \frac{(D/2)^2}{2} + m_2 \cdot L^2$$

③ Obtain the gripper's moment of inertia:

$$I_3 = m_3 \cdot \frac{a^2+b^2}{12} + m_3 \cdot L^2$$

④ Obtain the actual moment of inertia:

$$I = I_1 + I_2 + I_3$$

(m_1: mass of lever
m_2: mass of cylinder
m_3: mass of gripper)

Calculation Example

L = 0.2 m, øD = 0.06 m, a = 0.06 m, b = 0.03 m, m_1 = 0.5 kg, m_2 = 0.4 kg, m_3 = 0.2 kg

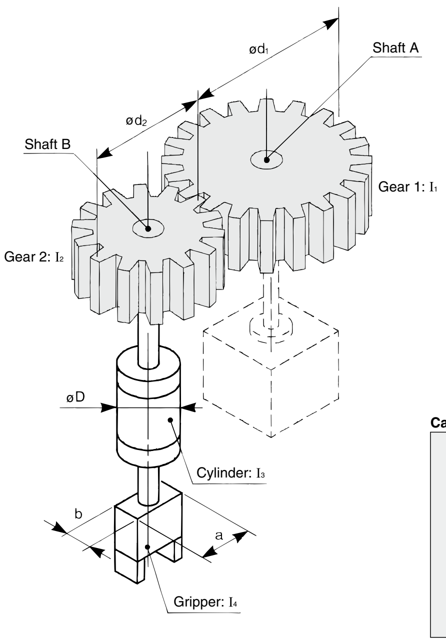
$I_1 = 0.5 \times \frac{0.2^2}{3} = 0.67 \times 10^{-2}$ kg·m²

$I_2 = 0.4 \times \frac{(0.06/2)^2}{8} + 0.4 \times 0.2^2 = 1.62 \times 10^{-2}$ kg·m²

$I_3 = 0.2 \times \frac{0.06^2 + 0.03^2}{12} + 0.2 \times 0.2^2 = 0.81 \times 10^{-2}$ kg·m²

$I = (0.67 + 1.62 + 0.81) \times 10^{-2} = 3.1 \times 10^{-2}$ kg·m²

4 If a load is rotated through the gears:



Example: ① Obtain the moment of inertia I_1 around shaft A:

$$I_1 = m_1 \cdot \frac{(d_1/2)^2}{2}$$

② Obtain moment of inertias I_2, I_3, and I_4 around shaft B:

$$I_2 = m_2 \cdot \frac{(d_2/2)^2}{2} \qquad I_3 = m_3 \cdot \frac{(D/2)^2}{2}$$

$$I_4 = m_4 \cdot \frac{a^2+b^2}{12} \qquad I_B = I_2 + I_3 + I_4$$

③ Replace the moment of inertia I_B around shaft B with the moment of inertia I_A around shaft A.

$I_A = (A/B)^2 \cdot I_B$ [A/B: ratio of the number of teeth]

④ Obtain the actual moment of inertia:

$$I = I_1 + I_A$$

(m_1: mass of gear 1
m_2: mass of gear 2
m_3: mass of cylinder
m_4: mass of gripper)

Calculation Example

d_1 = 0.1 m, d_2 = 0.05 m, D = 0.04 m, a = 0.04 m, b = 0.02 m
m_1 = 1 kg, m_2 = 0.4 kg, m_3 = 0.5 kg, m_4 = 0.2 kg, tooth count ratio = 2

$I_1 = 1 \times \frac{(0.1/2)^2}{8} = 1.25 \times 10^{-3}$ kg·m²

$I_2 = 0.4 \times \frac{(0.05/2)^2}{2} = 0.13 \times 10^{-3}$ kg·m²

$I_3 = 0.5 \times \frac{(0.04/2)^2}{2} = 0.1 \times 10^{-3}$ kg·m²

$I_4 = 0.2 \times \frac{0.04^2 + 0.02^2}{12} = 0.03 \times 10^{-3}$ kg·m²

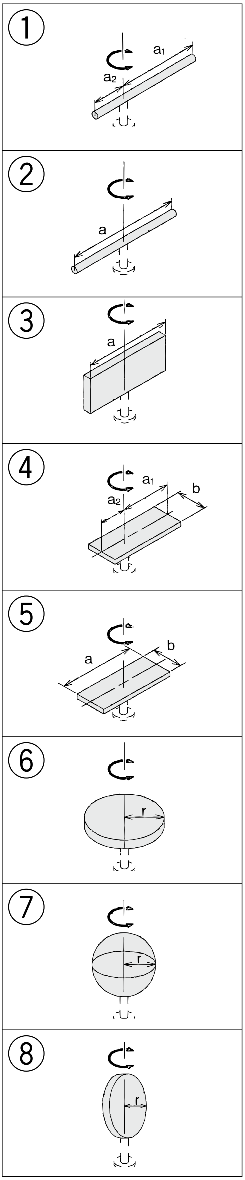
$I_B = (0.13 + 0.1 + 0.03) \times 10^{-3} = 0.26 \times 10^{-3}$ kg·m²

$I_A = 2^2 \times 0.26 \times 10^{-3} = 1.04 \times 10^{-3}$ kg·m²

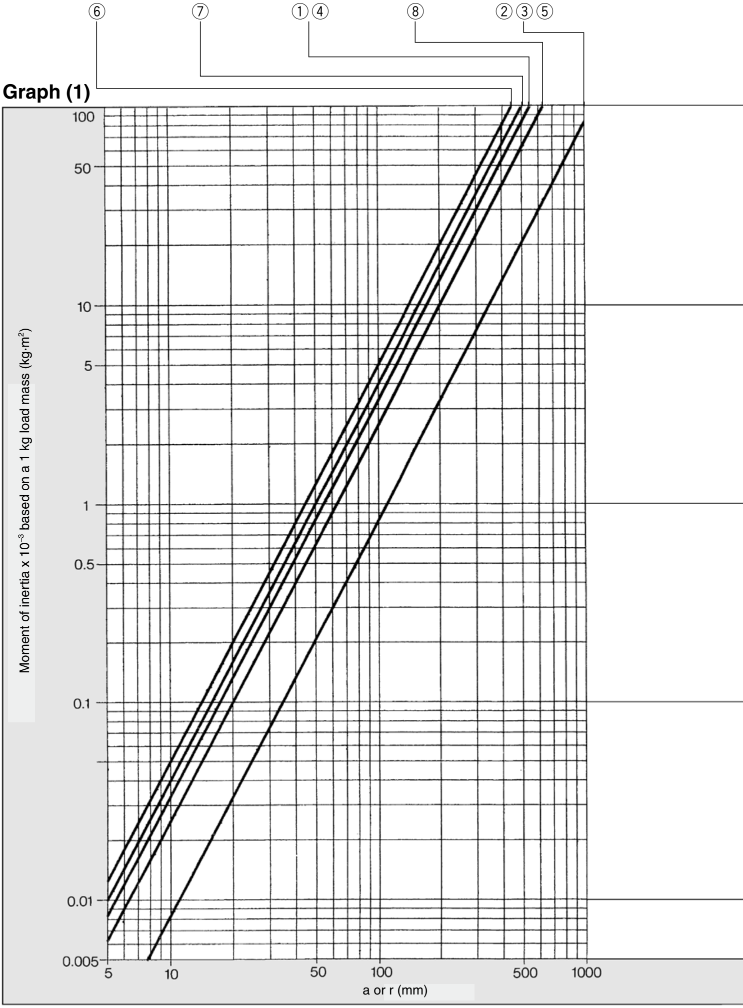
$I = (1.25 + 1.04) \times 10^{-3} = 2.29 \times 10^{-3}$ kg·m²

Rotary Actuators Model Selection

❶-3 Graph for Calculating the Moment of Inertia



Graph (1)



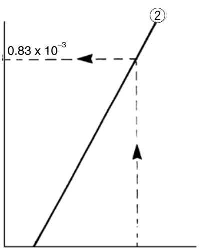
How to read the graph: only when the dimension of the load is "a" or "r"

[Example] When the load shape is ②, a = 100 mm, and the load mass is 0.1 kg.

In Graph (1), the point at which the vertical line of a = 100 mm and the line of the load shape ② intersect indicates that the moment of inertia of the 1 kg mass is 0.83×10^{-3} kg·m².

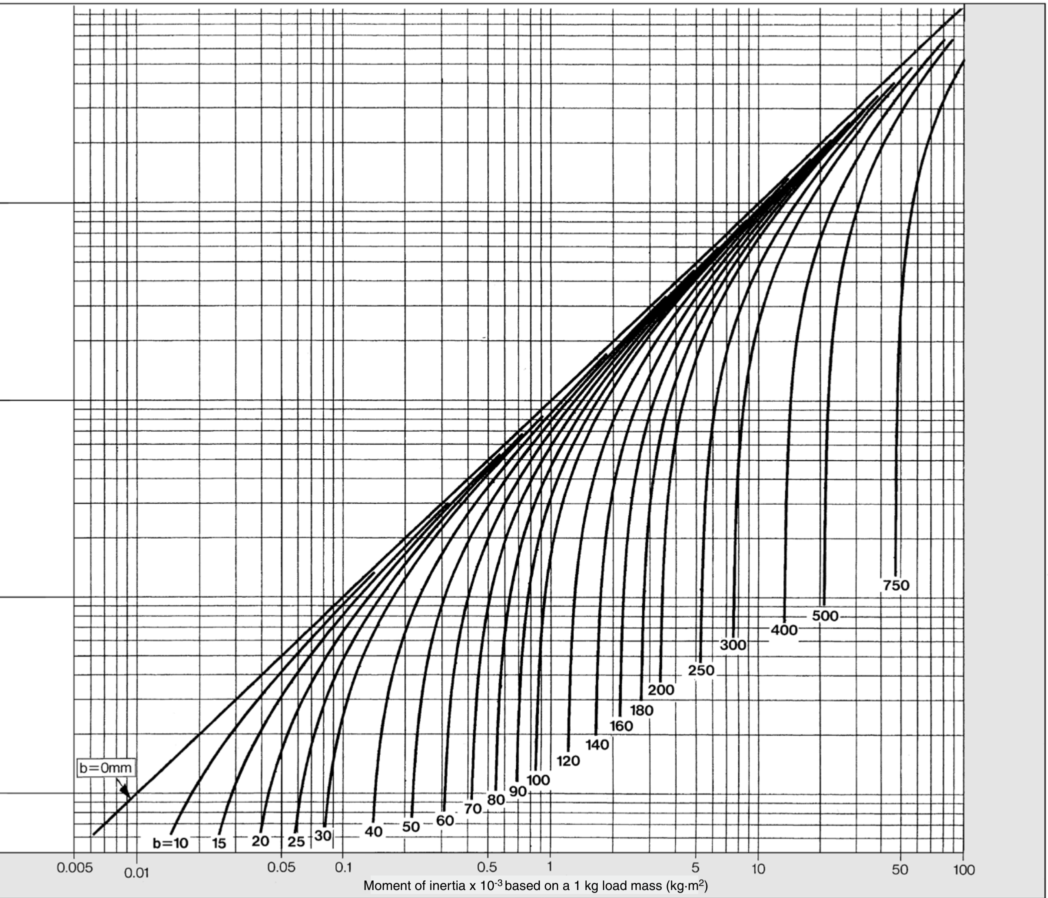
Because the mass of the load is 0.1 kg, the actual moment of inertia is $0.83 \times 10^{-3} \times 0.1 = 0.083 \times 10^{-3}$ kg·m².

(Note: If "a" is divided into "a¹a²", the moment of inertia can be obtained by calculating them separately.)



CRB2-Z
CRBU2
CRB1
MSU
CRJ
CRA1-Z
CRA1
CRQ2
MSQ
MSZ
CRQ2X MSQX
MRQ

Graph (2)

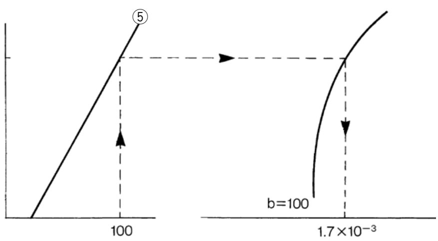


How to read the graph: when the dimension of the load contains both "a" and "b".

[Example] When the load shape is ⑤, a = 100 mm, b = 100 mm, and the load mass is 0.5 kg.

In Graph (1), obtain the point at which the vertical line of a = 100 mm and the line of the load shape ⑤ intersect. Move this intersection point to Graph (2), and the point at which it intersects with the curve of b = 100 mm indicates that the moment of inertia of the 1 kg mass is 1.7×10^{-3} kg·m².

Since the load mass is 0.5 kg, the actual moment of inertia is
$1.7 \times 10^{-3} \times 0.5 = 0.85 \times 10^{-3}$ kg·m².



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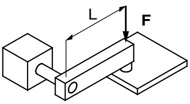
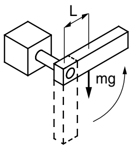
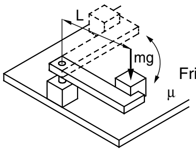
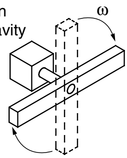
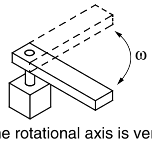
❷ Calculation of Required Torque

❷-1 Load Type

The calculation method of required torque varies depending on the load type. Obtain the required torque referring to the table below.

Load type		
Static load: Ts	**Resistance load: Tf**	**Inertial load: Ta**
When the pressing force is necessary (clamp, etc.)	When friction force or gravity is applied to the rotation direction	When the load with inertia is rotated
	Gravity acts   Friction force acts	The center of rotation and the center of gravity are corresponding   The rotational axis is vertical (up and down)
Ts = **F·L** Ts: Static load (N·m) F : Clamp force (N) L : Distance from the center of rotation to clamp (m)	When gravity acts to the rotation direction **Tf** = **m·g·L** When friction force acts to the rotation direction **Tf** = μ·**m·g·L** Tf : Resistance load (N·m) m : Mass of load (kg) g : Gravitational acceleration 9.8 (m/s^2) L : Distance from the center of rotation to the gravity or friction force acting point (m) μ : Coefficient of friction	**Ta** = $I \cdot \dot{\omega} = I \cdot \frac{2\theta}{t^2}$ Ta: Inertial load (N·m) I : Moment of inertia ($kg \cdot m^2$) $\dot{\omega}$: Angular acceleration (rad/s^2) θ : Rotating angle (rad) t : Rotation time (s)
Required torque **T** = **Ts**	Required torque **T** = **Tf** x (3 to 5) Note 1)	Required torque **T** = **Ta** x 10 Note 1)

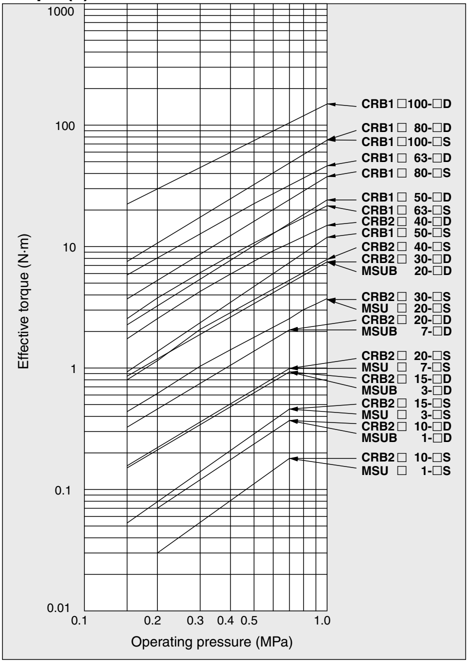
- Resistance loads → Gravity or friction applies in the rotation direction.
  Example 1) The axis of rotation is in a horizontal (lateral) direction, and the center of rotation and center of gravity of the load are not the same.
  Example 2) The load slips against the floor while rotating.
  *The necessary torque equals the total of the resistance load and inertial load.
  T = **Tf** x (3 to 5) + **Ta** x 10
- Non-resistance loads → Gravity or friction does not apply in the rotation direction.
  Example 1) The axis of rotation is in a perpendicular (vertical) direction.
  Example 2) The axis of rotation is in a horizontal (lateral) direction, and the center of rotation and center of gravity of the load are the same.
  *The necessary torque equals the inertial load only.
  T = **Ta** x 10

Note 1) In order to adjust the velocity, it is necessary to have a margin of adjustment for Tf and Ta.

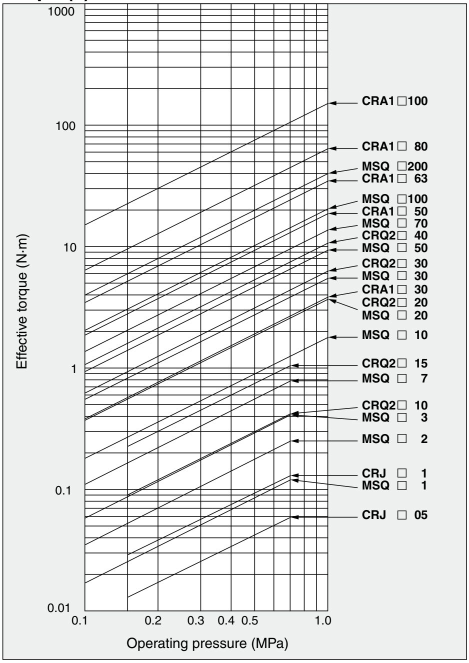
⇒P.31 Effective torque
⇒P.31 and 32 Effective torque for each equipment

❷-2 Effective Torque

Graph (3) Series CRB2/CRBU2/CRB1/MSU



Graph (4) Series CRA1/CRQ2/MSQ/CRJ

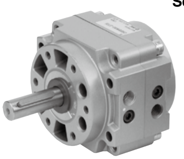


❷-3 Effective Torque for Each Equipment

Vane Style: Series CRB2□/CRBU2□/CRB1□


Series CRB2


Series CRBU2


Series CRB1

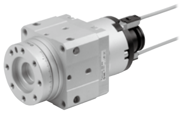
(N·m)

Size	Vane type	Operating pressure (MPa)									
		0.15	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0
10	Single vane	—	0.03	0.06	0.09	0.12	0.15	0.18	—	—	—
	Double vane	—	0.07	0.13	0.19	0.25	0.31	0.37	—	—	—
15	Single vane	0.06	0.10	0.17	0.24	0.32	0.39	0.46	—	—	—
	Double vane	0.13	0.20	0.34	0.48	0.65	0.79	0.93	—	—	—
20	Single vane	0.16	0.23	0.39	0.54	0.70	0.84	0.99	—	—	—
	Double vane	0.33	0.47	0.81	1.13	1.45	1.76	2.06	—	—	—
30	Single vane	0.44	0.62	1.04	1.39	1.83	2.19	2.58	3.03	3.40	3.73
	Double vane	0.90	1.26	2.10	2.80	3.70	4.40	5.20	6.09	6.83	7.49
40	Single vane	0.81	1.21	2.07	2.90	3.73	4.55	5.38	6.20	7.03	7.86
	Double vane	1.78	2.58	4.30	5.94	7.59	9.24	10.89	12.5	14.1	15.8
50	Single vane	1.20	1.86	3.14	4.46	5.69	6.92	8.14	9.5	10.7	11.9
	Double vane	2.70	4.02	6.60	9.21	11.8	14.3	16.7	19.4	21.8	24.2
63	Single vane	2.59	3.77	6.11	8.45	10.8	13.1	15.5	17.8	20.2	22.5
	Double vane	5.85	8.28	13.1	17.9	22.7	27.5	32.3	37.10	41.9	46.7
80	Single vane	4.26	6.18	10.4	14.2	18.0	21.9	25.7	30.0	33.8	37.6
	Double vane	8.70	12.6	21.1	28.8	36.5	44.2	51.8	60.4	68.0	75.6
100	Single vane	8.6	12.2	20.6	28.3	35.9	43.6	51.2	59.7	67.3	75
	Double vane	17.9	25.2	42.0	57.3	72.6	87.9	103	120	135	150

Rotary Actuators Model Selection

❷-3 Effective Torque for Each Equipment

Vane Style/Rotary Table: Series MSU□



Series MSUA

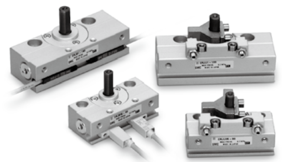
Series MSUB

(N·m)

Size	Vane type	Operating pressure (MPa)									
		0.15	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0
1	Single vane	–	0.03	0.06	0.09	0.11	0.14	0.17	–	–	–
	Double vane	–	0.06	0.12	0.18	0.23	0.29	0.35	–	–	–
3	Single vane	0.05	0.09	0.16	0.23	0.31	0.38	0.45	–	–	–
	Double vane	0.11	0.18	0.32	0.46	0.62	0.77	0.91	–	–	–
7	Single vane	0.14	0.21	0.37	0.52	0.69	0.83	0.98	–	–	–
	Double vane	0.29	0.44	0.78	1.10	1.42	1.74	2.04	–	–	–
20	Single vane	0.40	0.58	0.99	1.38	1.78	2.19	2.58	2.99	3.39	3.73
	Double vane	0.86	1.22	2.04	2.82	3.63	4.43	5.22	6.04	6.83	7.49

∗ Double vane type is Series MSUB only.

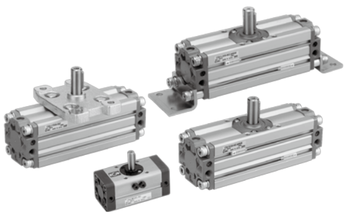
Rack & Pinion Style: Series CRJ□



(N·m)

Size	Operating pressure (MPa)						
	0.15	0.2	0.3	0.4	0.5	0.6	0.7
05	0.013	0.017	0.026	0.034	0.042	0.050	0.059
1	0.029	0.038	0.057	0.076	0.095	0.11	0.13

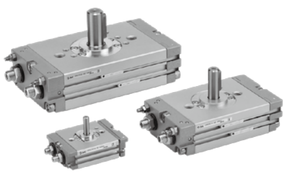
Rack & Pinion Style: Series CRA1□



(N·m)

Size	Operating pressure (MPa)									
	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	1.00
30	0.38	0.76	1.14	1.53	1.91	2.29	2.67	3.05	3.44	3.82
50	1.85	3.71	5.57	7.43	9.27	11.2	13.0	14.9	16.7	18.5
63	3.44	6.88	10.4	13.8	17.2	20.6	24.0	27.5	31.0	34.4
80	6.34	12.7	19.0	25.3	31.7	38.0	44.4	50.7	57.0	63.4
100	14.9	29.7	44.6	59.4	74.3	89.1	104	119	133	149

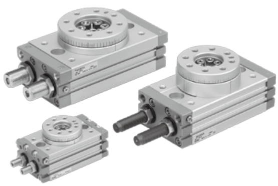
Rack & Pinion Style: Series CRQ2□



(N·m)

Size	Operating pressure (MPa)										
	0.10	0.15	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	1.00
10	–	0.09	0.12	0.18	0.24	0.30	0.36	0.42	–	–	–
15	–	0.22	0.30	0.45	0.60	0.75	0.90	1.04	–	–	–
20	0.37	0.55	0.73	1.10	1.47	1.84	2.20	2.57	2.93	3.29	3.66
30	0.62	0.94	1.25	1.87	2.49	3.11	3.74	4.37	4.99	5.60	6.24
40	1.06	1.59	2.11	3.18	4.24	5.30	6.36	7.43	8.48	9.54	10.6

Rack & Pinion Style/Rotary Table: Series MSQ□

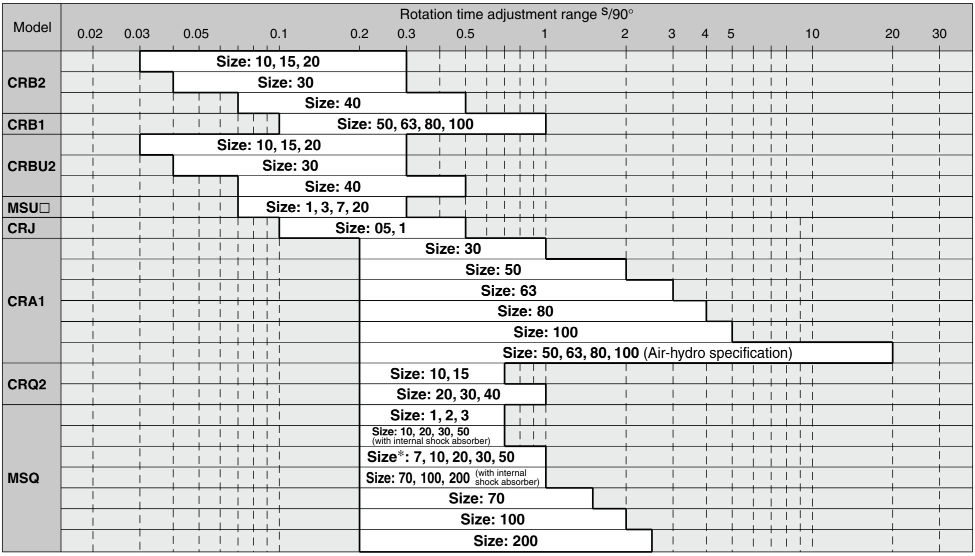


(N·m)

Size	Operating pressure (MPa)									
	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	1.00
1	0.017	0.035	0.052	0.070	0.087	0.10	0.12	–	–	–
2	0.035	0.071	0.11	0.14	0.18	0.21	0.25	–	–	–
3	0.058	0.12	0.17	0.23	0.29	0.35	0.41	–	–	–
7	0.11	0.22	0.33	0.45	0.56	0.67	0.78	–	–	–
10	0.18	0.36	0.53	0.71	0.89	1.07	1.25	1.42	1.60	1.78
20	0.37	0.73	1.10	1.47	1.84	2.20	2.57	2.93	3.29	3.66
30	0.55	1.09	1.64	2.18	2.73	3.19	3.82	4.37	4.91	5.45
50	0.93	1.85	2.78	3.71	4.64	5.57	6.50	7.43	8.35	9.28
70	1.36	2.72	4.07	5.43	6.79	8.15	9.50	10.9	12.20	13.6
100	2.03	4.05	6.08	8.11	10.1	12.2	14.2	16.2	18.20	20.3
200	3.96	7.92	11.9	15.8	19.8	23.8	27.7	31.7	35.60	39.6

❸ Confirmation of Rotation Time

Rotation time adjustment range is specified for each product for stable operation. Set the rotation time within the rotation time specified below.



*: In case of basic type/with external shock absorber.
If the product is used in a low speed range which is outside the adjustment range, it may cause the stick-slip phenomenon, or the product to stick or stop.

CRB2-Z
CRBU2
CRB1
MSU
CRJ
CRA1-Z
CRA1
CRQ2
MSQ
MSZ
CRQ2X MSQX
MRQ
D-□

❹ Calculation of Kinetic Energy

Kinetic energy is generated when the load rotates. Kinetic energy applies on the product at the operating end as inertial force, and may cause the product to damage. In order to avoid this, the value of allowable kinetic energy is determined for each product.
Find the kinetic energy of the load, and verify that it is within the allowable range for the product in use.

Kinetic Energy

Use the following formula to calculate the kinetic energy of the load.

$$E = \frac{1}{2} \cdot I \cdot \omega^2$$

E: Kinetic energy (J)
I: Moment of inertia (kg·m²)
ω: Angle speed (rad/s)

∗ For the MSU Series, add the values shown in the table below to the moment of inertia of the load when calculating.

Model	Additional value of moment of inertia; I_0
MSU□ 1	2.5×10^{-6}
MSU□ 3	6.2×10^{-6}
MSU□ 7	1.6×10^{-5}
MSU□20	2.8×10^{-5}

Kinetic energy formula for Series MSU

$$E = \frac{1}{2} (I + I_0)\, \omega^2$$

Angle Speed

$$\omega = \frac{2\theta}{t}$$

ω: Angle speed (rad/s)
θ: Rotation angle (rad)
t: Rotation time (s)

However, for the air-hydro type, when the rotation time for 90° becomes longer than 2 seconds, use the following formula.

$$\omega = \frac{\theta}{t}$$

⇒P.35 Allowable kinetic energy and rotation time adjustment range
⇒P.36 to 38 Moment of inertia and rotation time

To find the rotation time when kinetic energy is within the allowable range for the product, use the following formula.

When the rotation angle is $\omega = \frac{2\theta}{t}$

$$t \geq \sqrt{\frac{2 \cdot I \cdot \theta^2}{E}}$$

When the rotation angle is $\omega = \frac{\theta}{t}$

$$t \geq \sqrt{\frac{I \cdot \theta^2}{2E}}$$

t: Rotation time (s)
I: Moment of inertia (kg·m²)
θ: Rotation angle (rad)
E: Kinetic energy (J)

❹-1 Allowable Kinetic Energy and Rotation Time Adjustment Range

Table (1a) Allowable Kinetic Energy and Rotation Time Adjustment Range of the Single Vane

Model	Allowable kinetic energy (J)		Adjustable range of rotation time safe in operation (S/90°)
	Without rubber bumper	With rubber bumper	
CRB2 □ 10	0.00015	—	0.03 to 0.3
CRB2 □ 15	0.00025	0.001	
CRB2 □ 20	0.00040	0.003	
CRB2 □ 30	0.015	0.020	0.04 to 0.3
CRB2 □ 40	0.030	0.040	0.07 to 0.5
CRB1 □ 50	0.082		0.1 to 1
CRB1 □ 63	0.120		
CRB1 □ 80	0.398		
CRB1 □100	0.600		
CRBU2□ 10	0.00015	—	0.03 to 0.3
CRBU2□ 15	0.00025	0.001	
CRBU2□ 20	0.0004	0.003	
CRBU2□ 30	0.015	0.02	0.04 to 0.3
CRBU2□ 40	0.030	0.040	0.07 to 0.5
MSUA 1	0.0065	—	0.07 to 0.3
MSUA 3	0.017	—	
MSUA 7	0.042	—	
MSUA 20	0.073	—	
MSUB 1	0.005	—	
MSUB 3	0.013	—	
MSUB 7	0.032	—	
MSUB 20	0.056	—	

Table (1b) Allowable Kinetic Energy and Rotation Time Adjustment Range of the Double Vane

Model	Allowable kinetic energy (J)		Adjustable range of rotation time safe in operation (S/90°)
	Without rubber bumper	With rubber bumper	
CRB2 □ 10	0.0003	—	0.03 to 0.3
CRB2 □ 15	0.0005	0.0012	
CRB2 □ 20	0.0007	0.0033	
CRB2 □ 30	0.015	0.020	0.04 to 0.3
CRB2 □ 40	0.030	0.040	0.07 to 0.5
CRB1 □ 50	0.112		0.1 to 1
CRB1 □ 63	0.160		
CRB1 □ 80	0.540		
CRB1 □100	0.811		
CRBU2□ 10	0.0003	—	0.03 to 0.3
CRBU2□ 15	0.0005	0.0012	
CRBU2□ 20	0.0007	0.0033	
CRBU2□ 30	0.015	0.020	0.04 to 0.3
CRBU2□ 40	0.030	0.040	0.07 to 0.5
MSUB 1	0.005	—	0.07 to 0.3
MSUB 3	0.013	—	
MSUB 7	0.032	—	
MSUB 20	0.056	—	

Note) Not using rubber bumper means that the rotary actuator is stopped in the middle of its rotation through the use of an external stopper.
Note) Using a rubber bumper means that the rotary actuator is stopped at the respective rotation ends by using an internal stopper.

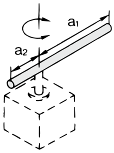
Table (2) Allowable Kinetic Energy and Rotation Time Adjustment Range

Model	Allowable kinetic energy (J)		Cushion angle	Adjustable range of rotation time safe in operation (S/90°)
	Without rubber bumper	With rubber bumper		
CRJ □ 05	0.00025	—	—	0.1 to 0.5
	0.001 *1	—	—	
CRJ □ 1	0.00040	—	—	
	0.002 *1	—	—	
CRA1□ 30	0.010	—	—	0.2 to 1
CRA1□ 50	0.050	0.980 *2	35°	0.2 to 2
CRA1□ 63	0.120	1.500 *2		0.2 to 3
CRA1□ 80	0.160	2.000 *2		0.2 to 4
CRA1□100	0.540	2.900 *2		0.2 to 5
CRQ2□ 10	0.00025	—	—	0.2 to 0.7
CRQ2□ 15	0.00039	—	—	
CRQ2□ 20	0.025	0.120 *2	40°	0.2 to 1
CRQ2□ 30	0.048	0.250 *2		
CRQ2□ 40	0.081	0.400 *2		
MSQ □ 1	0.001	—	—	0.2 to 0.7
MSQ □ 2	0.0015	—	—	
MSQ □ 3	0.002	—	—	
MSQ □ 7	0.006	—	—	0.2 to 1
MSQ □ 10	0.007	0.039 *3	52°	0.2 to 0.7 *3
		0.161 *4	7.1°	
		0.231 *5	8.6°	0.2 to 1
MSQ □ 20	0.025	0.116 *3	43°	0.2 to 0.7 *3
		0.574 *4	6.9°	
		1.060 *5	8.0°	0.2 to 1
MSQ □ 30	0.048	0.116 *3	40°	0.2 to 0.7 *3
		0.805 *4	6.2°	
		1.210 *5	7.3°	0.2 to 1
MSQ □ 50	0.081	0.294 *3	60°	0.2 to 0.7 *3
		1.310 *4	9.6°	
		1.820 *5	10.5°	0.2 to 1
MSQB 70	0.24	1.100 *3	71°	0.2 to 1.5 / 0.2 to 1 *3
MSQB 100	0.32	1.600 *3	62°	0.2 to 2
MSQB 200	0.56	2.900 *3	82°	0.2 to 2.5

*1 Represents external stopper.
*2 When the cushion needle with air cushion is adjusted optimally.
*3 Represents internal shock absorber.
*4 Represents external and low energy type shock absorber.
*5 Represents external and high energy type shock absorber.

Calculation Example

Load form: Round rod
Length of a_1 part: 0.12 m Rotation angle : 90°
Length of a_2 part: 0.04 m Rotation time : 0.9 S/90°
Mass of a_1 part (= m_1): 0.09 kg
Mass of a_2 part (= m_2): 0.03 kg



$$I = m_1 \cdot \frac{a_1^2}{3} + m_2 \cdot \frac{a_2^2}{3}$$

(Step 1) Find the angle speed ω.

$$\omega = \frac{2\theta}{t} = \frac{2}{0.9}\left(\frac{\pi}{2}\right)$$

$= 3.489$ rad/s

(Step 2) Find the moment of inertia I.

$$I = \frac{m_1 \cdot a_1^2}{3} + \frac{m_2 \cdot a_2^2}{3}$$

$$= \frac{0.09 \times 0.12^2}{3} + \frac{0.03 \times 0.04^2}{3}$$

$= 4.48 \times 10^{-4}$ kg·m²

(Step 3) Find the kinetic energy E.

$$E = \frac{1}{2} \cdot I \cdot \omega^2 = \frac{1}{2} \times 4.48 \times 10^{-4} \times 3.489^2$$

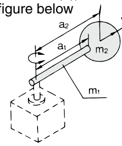
$= 0.00273$ J

Calculation Example

If the model to be used has been determined, obtain the threshold rotation time in which the rotary actuator can be used in accordance with the allowable kinetic energy of that model.

Model used : CRA1□□50 (Without bumper)
Allowable kinetic energy : 0.05 J (Refer to Table (2))
Load form : Refer to the figure below
Rotation angle : 90°

$$I = m_1 \cdot \frac{a_1^2}{3} + m_2 \cdot a_2^2 + m_2 \cdot \frac{2r^2}{5}$$



a_1 : 0.12 m
a_2 : 0.15 m
m_1 : 0.1 kg
m_2 : 0.18 kg
r : 0.03 m

(Step 1) Find the moment of inertia.

$$I = \frac{m_1 \cdot a_1^2}{3} + m_2 \cdot a_2^2 + \frac{m_2 \cdot 2r^2}{5}$$

$$= \frac{0.1 \times 0.12^2}{3} + 0.18 \times 0.15^2 + \frac{0.18 \times 2 \times 0.03^2}{5}$$

$= 4.6 \times 10^{-3}$ kg·m²

(Step 2) Find the rotating time.

$$t \geq \sqrt{\frac{2 \cdot I \cdot \theta^2}{E}} = \sqrt{\frac{2 \times 4.6 \times 10^{-3} \times (\pi/2)^2}{0.05}} = 0.67\text{s}$$

It is therefore evident that there will be no problem if it is used with a rotation time of less than 0.67s. However, according to table 2, the maximum value of rotation time for stable operation is 2s. Thus, the rotation time should be within the range of $0.67 \leq t \leq 2$.

❹-2 Moment of Inertia and Rotation Time

How to read the graph

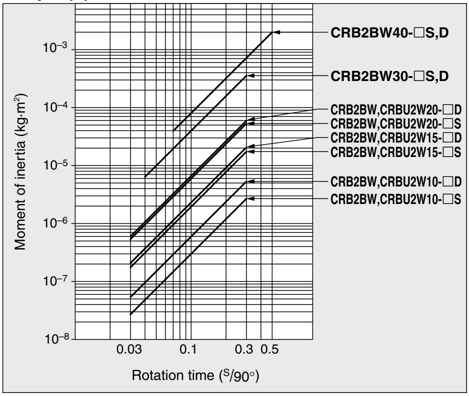
Example 1) When there are constraints for the moment of inertia of load and rotation time. From "Graph (5)", to operate at the load moment of inertia 1 x 10^{-4} kg·m^2 and at the rotation time setting of 0.3 S/90°, the models will be CRB□30–□S and CRB□30–□D.

Example 2) When there are constraints for the moment of inertia of load, but not for rotation time. From "Graph (6)", to operate at the load moment of inertia 1 x 10^{-2} kg·m^2:
CRB1□50–□S will be 0.8 to 1 S/90°
CRB1□80–□S will be 0.35 to 1 S/90°
CRB1□100–□S will be 0.29 to 1 S/90°

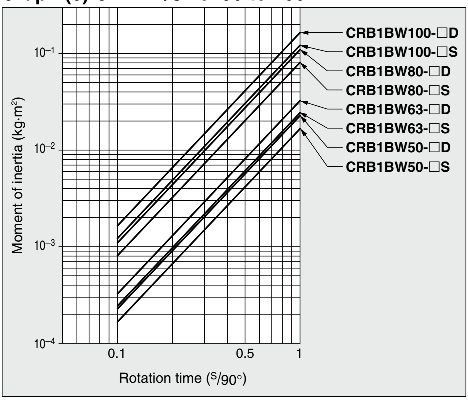
[Remarks] As for the rotation times in "Graphs (5) to (15)", the lines in the graph indicate the adjustable speed ranges. If the speed is adjusted towards the low-speed end beyond the range of the line, it could cause the actuator to stick, or, in the case of the vane style, it could stop its operation.

<Vane style: Series CRB2/CRBU2/CRB1/MSU>

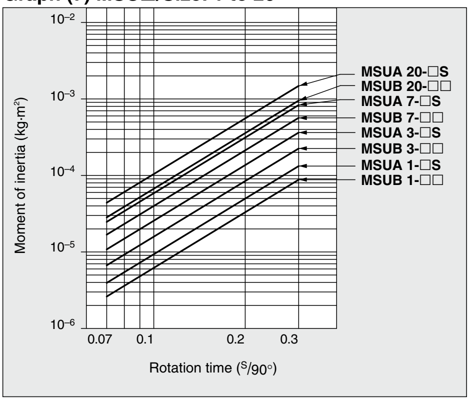
Graph (5) CRB2□, CRBU2□/Size: 10 to 40



Graph (6) CRB1□/Size: 50 to 100

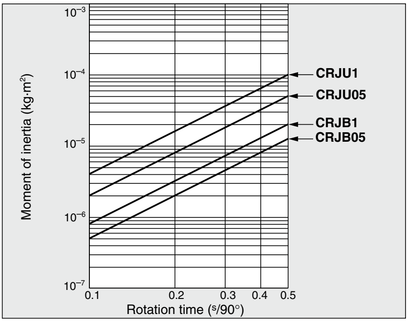


Graph (7) MSU□/Size: 1 to 20

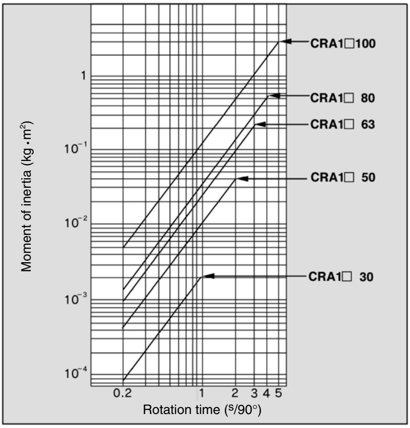


<Rack & pinion style: Series CRJ/CRA1>

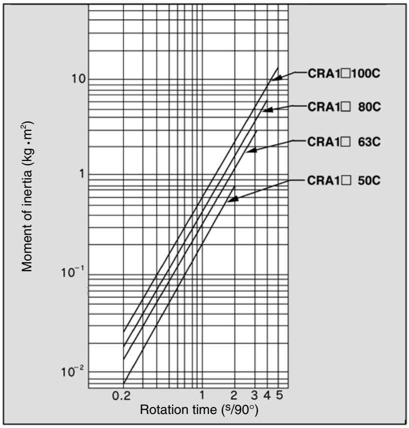
Graph (8) CRJ□/Size: 05, 1



Graph (9) CRA1□/Size: 30 to 100 (Without cushion)

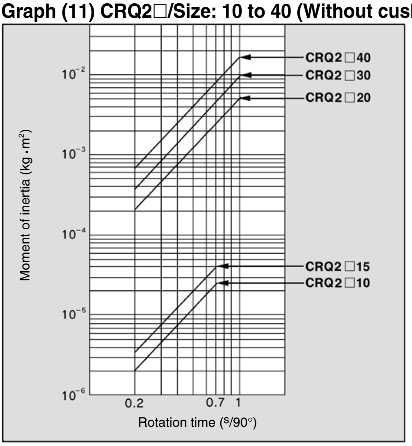


Graph (10) CRA1□/Size: 50 to 100 (With cushion)

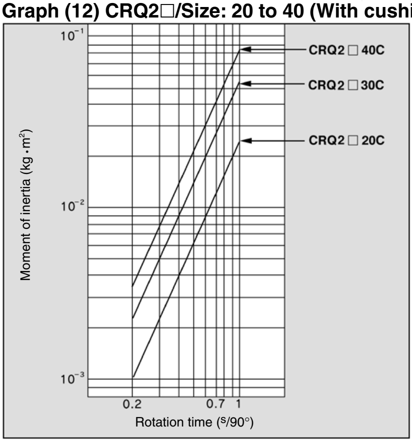


<Rack & pinion style: Series CRQ2/MSQ>

Graph (11) CRQ2□/Size: 10 to 40 (Without cushion)



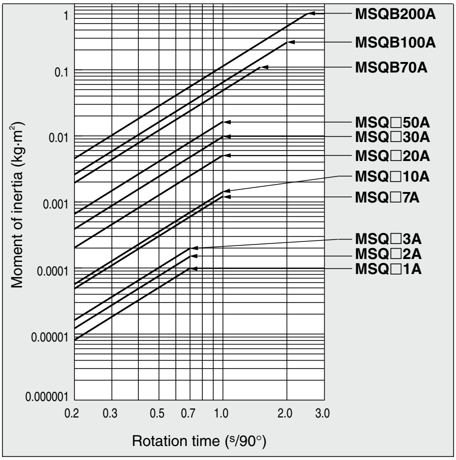
Graph (12) CRQ2□/Size: 20 to 40 (With cushion)



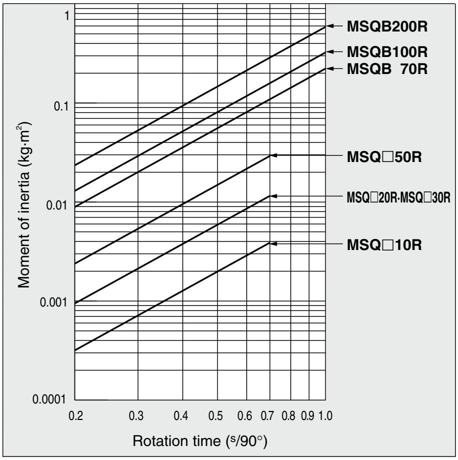
CRB2 -Z
CRBU2
CRB1
MSU
CRJ
CRA1 -Z
CRA1
CRQ2
MSQ
MSZ
CRQ2X MSQX
MRQ
D-□

❹-2 Moment of Inertia and Rotation Time

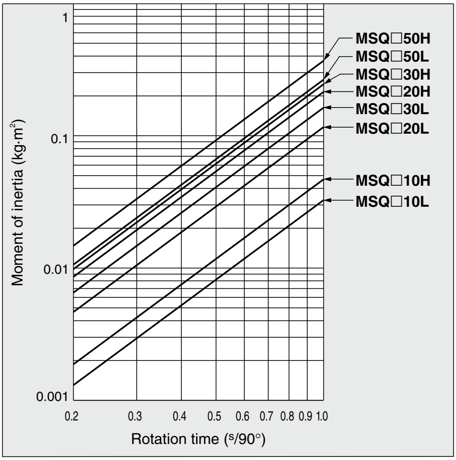
Graph (13) MSQ□/Size: 10 to 200 (Adjust bolt type)



Graph (14) MSQ□/Size: 10 to 200 (Internal absorber type)



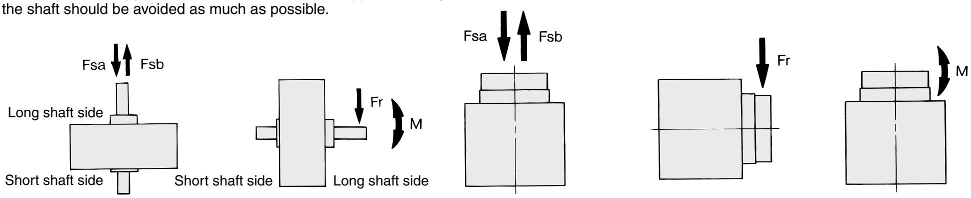
Graph (15) MSQ□/Size: 10 to 50 (External absorber type)



CRB2
-Z
CRBU2
CRB1
MSU
CRJ
CRA1
-Z
CRA1
CRQ2
MSQ
MSZ
CRQ2X
MSQX
MRQ
D-□

❺ Confirmation of Allowable Load

Provided that a dynamic load is not generated, a load in the axial direction can be applied up to the value that is indicated in the table below. However, applications in which the load is applied directly to the shaft should be avoided as much as possible.



Vane Style

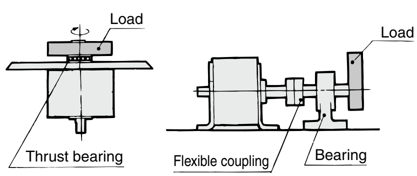
Vane Style (Single, Double)

Series	Model	Load direction			
		Fsa (N)	Fsb (N)	Fr (N)	M (N·m)
CRB	CRB2 □ 10	9.8	9.8	14.7	0.13
	CRB2 □ 15	9.8	9.8	14.7	0.17
	CRB2 □ 20	19.6	19.6	24.5	0.33
	CRB2 □ 30	24.5	24.5	29.4	0.42
	CRB2 □ 40	40	40	60	1.02
	CRB1 □ 50	196	196	245	8.09
	CRB1 □ 63	340	340	390	14.04
	CRB1 □ 80	490	490	490	20.09
	CRB1 □100	539	539	588	30.28
CRBU2	CRBU2□ 10	9.8	9.8	14.7	0.13
	CRBU2□ 15	9.8	9.8	14.7	0.17
	CRBU2□ 20	19.6	19.6	24.5	0.33
	CRBU2□ 30	24.5	24.5	29.4	0.42
	CRBU2□ 40	40	40	60	1.02

Vane Style (Single, Double)

Series	Model	Load direction			
		Fsa (N)	Fsb (N)	Fr (N)	M (N·m)
MSUA	MSUA 1	15	15	20	0.3
	MSUA 3	30	30	40	0.7
	MSUA 7	60	60	50	0.9
	MSUA20	80	80	60	2.9
MSUB	MSUB 1	10	15	20	0.3
	MSUB 3	15	30	40	0.7
	MSUB 7	30	60	50	0.9
	MSUB20	40	80	60	2.9

Provided that a dynamic load is not generated, a load that is within the allowable radial/thrust load can be applied. However, applications in which the load is applied directly to the shaft should be avoided as much as possible. The methods such as those described below are recommended to prevent the load from being applied directly to the shaft in order to ensure a proper operating condition.



Rack & Pinion Style

Rack & Pinion Style (Single rack)

Series	Model	Load direction			
		Fsa (N)	Fsb (N)	Fr (N)	M (N·m)
CRJ	CRJ□ 05	20	20	25	0.26
	CRJ□ 1	25	25	30	0.32

Rack & Pinion Style (Single rack)

Series	Model	Load direction			
		Fsa (N)	Fsb (N)	Fr (N)	M (N·m)
CRA1	CRA1□ 30	29.4	29.4	29.4	0.44
	CRA1□ 50	490	196	196	3.63
	CRA1□ 63	588	196	294	6.17
	CRA1□ 80	882	196	392	9.80
	CRA1□100	980	196	588	19.11

Rack & Pinion Style (Double rack)

Series	Model	Load direction			
		Fsa (N)	Fsb (N)	Fr (N)	M (N·m)
CRQ2	CRQ2B□10	15.7	7.8	14.7	0.21
	CRQ2B□15	19.6	9.8	19.6	0.32
	CRQ2B□20	49	29.4	49	0.96
	CRQ2B□30	98	49	78	1.60
	CRQ2B□40	108	59	98	2.01

Rack & Pinion Style (Double rack)

Series	Model	Load direction			
		Fsa (N)	Fsb (N)	Fr (N)	M (N·m)
MSQA	MSQA 1□	41	41	31	0.84
	MSQA 2□	45	45	32	1.2
	MSQA 3□	48	48	33	1.6
	MSQA 7□	71	71	54	2.2
	MSQA 10□	107	74	86	2.9
	MSQA 20□	197	137	166	4.8
	MSQA 30□	398	197	233	6.4
	MSQA 50□	517	296	378	12.0
MSQB	MSQB 1□	41	41	31	0.56
	MSQB 2□	45	45	32	0.82
	MSQB 3□	48	48	33	1.1
	MSQB 7□	71	71	54	1.5
	MSQB 10□	78	74	78	2.4
	MSQB 20□	137	137	147	4.0
	MSQB 30□	363	197	196	5.3
	MSQB 50□	451	296	314	9.7
	MSQB 70□	476	296	333	12.0
	MSQB100□	708	493	390	18.0
	MSQB200□	1009	740	543	25.0

❻ Calculation of Air Consumption and Required Air Flow Capacity

Air consumption is the volume of air which is expended by the rotary actuator's reciprocal operation inside the actuator and in the piping between the actuator and the switching valve, etc. This is necessary for selection of a compressor and for calculation of its running cost.
Required air volume is the air volume necessary to make a rotary actuator operate at a required speed. It requires calculation when selecting the upstream piping diameter from the switching valve and air line equipment.

∗ To facilitate your calculation, Tables (1) to (5) provide the air consumption volume (Q_{CR}) that is required each time an individual rotary actuator makes a reciprocal movement.

1. Air consumption volume

Formula

Regarding QCR: With vane style sizes 10 to 40, use formula (1) because the internal volume varies when ports A and B are pressurized. For vane style sizes 50 to 100, as well as for the rack and pinion style, use formula (2).

$$Q_{CR} = (V_A + V_B) \times \left(\frac{P + 0.1}{0.1}\right) \times 10^{-3} \quad \cdots (1)$$

$$Q_{CR} = 2 \times V_A \times \left(\frac{P + 0.1}{0.1}\right) \times 10^{-3} \quad \cdots (2)$$

$$Q_{CP} = 2 \times a \times L \times \left(\frac{P}{0.1}\right) \times 10^{-6} \quad \cdots (3)$$

$$Q_C = Q_{CR} + Q_{CP} \quad \cdots (4)$$

Q_{CR} = Amount of air consumption of rotary actuator [L(ANR)]
Q_{CP} = Amount of air consumption of tube or piping [L(ANR)]
V_A = Inner volume of the rotary actuator (when pressurized from A port) [cm^3]
V_B = Inner volume of the rotary actuator (when pressurized from B port) [cm^3]
P = Operating pressure [MPa]
L = Length of piping [mm]
a = Inner sectional area of piping [mm^2]
Q_C = Amount of air consumption required for one cycle of the rotary actuator [L(ANR)]

To select a compressor, it is important to select one that has plenty of margin to accommodate the total air volume that is consumed by the pneumatic actuators that are located downstream. The total air consumption volume is affected by the leakage in the tube, the consumption in the drain valves and pilot valves, as well as by the reduction in air volume due to reduced temperature.

Formula

$$Q_{c2} = Q_c \times n \times \text{No. of actuators} \times \text{Space rate} \quad \cdots (5)$$

Q_{c2} = Amount of air from a compressor [L/min (ANR)]
n = Actuator reciprocations per minute

Safety factor: from 1.5

2. Required air flow capacity

Formula

Qr: Make use of (6)(7) formula for vane type, and (7) for rack and pinion type.

$$Q_r = \left\{V_B \times \left(\frac{P + 0.1}{0.1}\right) \times 10^{-3} + a \times L \times \left(\frac{P}{0.1}\right) \times 10^{-6}\right\} \times \frac{60}{t} \quad \cdots (6)$$

$$Q_r = \left\{V_A \times \left(\frac{P + 0.1}{0.1}\right) \times 10^{-3} + a \times L \times \left(\frac{P}{0.1}\right) \times 10^{-6}\right\} \times \frac{60}{t} \quad \cdots (7)$$

Q_r = Consumed air volume for rotary actuator [L/min(ANR)]
V_A = Inner volume of the rotary actuator (when pressurized from A port) [cm^3]
V_B = Inner volume of the rotary actuator (when pressurized from B port) [cm^3]
P = Operating pressure [MPa]
L = Length of piping [mm]
a = Inner sectional area of piping [mm^2]
t = Total time for rotation [S]

Internal Cross Section of Tubing and Steel Piping

Nominal	O.D. (mm)	I.D. (mm)	Internal cross section a (mm^2)
T□0425	4	2.5	4.9
T□0604	6	4	12.6
TU 0805	8	5	19.6
T□0806	8	6	28.3
1/8B	—	6.5	33.2
T□1075	10	7.5	44.2
TU 1208	12	8	50.3
T□1209	12	9	63.6
1/4B	—	9.2	66.5
TS 1612	16	12	113
3/8B	—	12.7	127
T□1613	16	13	133
1/2B	—	16.1	204
3/4B	—	21.6	366
1B	—	27.6	598

⇒P.41 and 42 Inner volume and air consumption
⇒P.43 and 44 Air consumption calculation graph

❻-1 Inner Volume and Air Consumption

Table (1) Vane Style: Series CRB2/CRBU2/CRB1

(L(ANR))

Vane	Size	Rotation (degree)	Inner volume (cm^3)		Operating pressure (MPa)									
			Press. V_A port	Press. V_B port	0.15	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0
Single vane	10	90	0.6	1.0	—	0.005	0.006	0.008	0.010	0.011	0.013	—	—	—
		180	1.2	1.2	—	0.007	0.010	0.012	0.014	0.017	0.019	—	—	—
		270	1.5	1.5	—	0.009	0.012	0.015	0.018	0.021	0.024	—	—	—
	15	90	1.0	1.5	0.006	0.008	0.010	0.013	0.015	0.018	0.020	—	—	—
		180	2.9	2.9	0.015	0.017	0.023	0.029	0.035	0.041	0.046	—	—	—
		270	3.7	3.7	0.019	0.022	0.030	0.037	0.044	0.052	0.059	—	—	—
	20	90	3.6	4.8	0.021	0.025	0.034	0.042	0.050	0.059	0.067	—	—	—
		180	6.1	6.1	0.031	0.037	0.049	0.061	0.073	0.085	0.098	—	—	—
		270	7.9	7.9	0.040	0.047	0.063	0.079	0.095	0.111	0.126	—	—	—
	30	90	8.5	11.3	0.050	0.059	0.079	0.099	0.119	0.139	0.158	0.178	0.198	0.218
		180	15	15	0.075	0.090	0.120	0.150	0.180	0.210	0.240	0.270	0.300	0.330
		270	20.2	20.2	0.101	0.121	0.162	0.202	0.242	0.283	0.323	0.364	0.404	0.444
	40	90	21	25	0.115	0.138	0.184	0.230	0.276	0.322	0.368	0.414	0.460	0.506
		180	31.5	31.5	0.158	0.189	0.252	0.315	0.378	0.441	0.504	0.567	0.630	0.693
		270	41	41	0.205	0.246	0.328	0.410	0.492	0.574	0.656	0.738	0.820	0.902
	50	90	30	30	0.150	0.180	0.240	0.300	0.360	0.420	0.480	0.540	0.600	0.660
		100	32	32	0.160	0.192	0.256	0.320	0.384	0.448	0.512	0.576	0.640	0.704
		180	49	49	0.245	0.294	0.392	0.490	0.588	0.686	0.784	0.882	0.980	1.078
		190	51	51	0.255	0.306	0.408	0.510	0.612	0.714	0.816	0.918	1.020	1.122
		270	66	66	0.330	0.396	0.528	0.660	0.792	0.924	1.056	1.188	1.320	1.452
		280	68	68	0.340	0.408	0.544	0.680	0.816	0.952	1.088	1.224	1.360	1.496
	63	90	70	70	0.350	0.420	0.560	0.700	0.840	0.980	1.120	1.260	1.400	1.540
		100	73	73	0.365	0.438	0.584	0.730	0.876	1.022	1.168	1.314	1.460	1.606
		180	94	94	0.470	0.564	0.752	0.940	1.128	1.316	1.504	1.692	1.880	2.068
		190	97	97	0.485	0.582	0.776	0.970	1.164	1.358	1.552	1.746	1.940	2.134
		270	118	118	0.590	0.708	0.944	1.180	1.416	1.652	1.888	2.124	2.360	2.596
		280	121	121	0.605	0.726	0.968	1.210	1.452	1.694	1.936	2.178	2.420	2.662
	80	90	88	88	0.440	0.528	0.704	0.880	1.056	1.232	1.408	1.584	1.760	1.936
		100	93	93	0.465	0.558	0.744	0.930	1.116	1.302	1.488	1.674	1.860	2.046
		180	138	138	0.690	0.828	1.104	1.380	1.656	1.932	2.208	2.484	2.760	3.036
		190	143	143	0.715	0.858	1.144	1.430	1.716	2.002	2.288	2.574	2.860	3.146
		270	188	188	0.940	1.128	1.504	1.880	2.256	2.632	3.008	3.384	3.760	4.136
		280	193	193	0.965	1.158	1.544	1.930	2.316	2.702	3.088	3.474	3.860	4.246
	100	90	186	186	0.930	1.116	1.488	1.860	2.232	2.604	2.976	3.348	3.720	4.092
		100	197	197	0.985	1.182	1.576	1.970	2.364	2.758	3.152	3.546	3.940	4.334
		180	281	281	1.405	1.686	2.248	2.810	3.372	3.934	4.496	5.058	5.620	6.182
		190	292	292	1.460	1.752	2.336	2.920	3.504	4.088	4.672	5.256	5.840	6.424
		270	376	376	1.880	2.256	3.008	3.760	4.512	5.264	6.016	6.768	7.520	8.272
		280	387	387	1.935	2.322	3.096	3.870	4.644	5.418	6.192	6.966	7.740	8.514
Double vane	10	90	1.0	1.0	—	0.006	0.008	0.010	0.012	0.014	0.016	—	—	—
		100	1.1	1.1	—	0.007	0.009	0.011	0.013	0.015	0.018	—	—	—
	15	90	2.6	2.6	0.013	0.016	0.021	0.026	0.031	0.036	0.042	—	—	—
		100	2.7	2.7	0.014	0.016	0.022	0.027	0.032	0.038	0.043	—	—	—
	20	90	5.6	5.6	0.028	0.034	0.045	0.056	0.067	0.078	0.090	—	—	—
		100	5.7	5.7	0.029	0.034	0.046	0.057	0.068	0.080	0.091	—	—	—
	30	90	14.4	14.4	0.072	0.086	0.115	0.144	0.173	0.202	0.230	0.259	0.288	0.317
		100	14.5	14.5	0.073	0.087	0.116	0.145	0.174	0.203	0.232	0.261	0.290	0.319
	40	90	33	33	0.165	0.198	0.264	0.330	0.396	0.462	0.528	0.594	0.660	0.726
		100	34	34	0.170	0.204	0.272	0.340	0.408	0.476	0.544	0.612	0.680	0.748
	50	90	48	48	0.240	0.288	0.384	0.480	0.576	0.672	0.768	0.864	0.960	1.056
		100	52	52	0.260	0.312	0.416	0.520	0.624	0.728	0.832	0.936	1.040	1.144
	63	90	98	98	0.490	0.588	0.784	0.980	1.176	1.372	1.568	1.764	1.960	2.156
		100	104	104	0.520	0.624	0.832	1.040	1.248	1.456	1.664	1.872	2.080	2.288
	80	90	136	136	0.680	0.816	1.088	1.360	1.632	1.904	2.176	2.448	2.720	2.992
		100	146	146	0.730	0.876	1.168	1.460	1.752	2.044	2.336	2.628	2.920	3.212
	100	90	272	272	1.360	1.632	2.176	2.720	3.264	3.808	4.352	4.896	5.440	5.984
		100	294	294	1.470	1.764	2.352	2.940	3.528	4.116	4.704	5.292	5.880	6.468

Table (2) Vane Style Rotary Table: Series MSU□

(L(ANR))

Vane	Size	Rotation (degree)	Inner volume (cm^3)		Operating pressure (MPa)									
			Press. V_A port	Press. V_B port	0.15	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0
Single vane	1	90	0.8	1.3	—	0.006	0.008	0.011	0.013	0.015	0.017	—	—	—
		180	1.3	1.3	—	0.008	0.010	0.013	0.016	0.018	0.021	—	—	—
	3	90	1.9	3.1	0.013	0.015	0.020	0.025	0.030	0.035	0.040	—	—	—
		180	3.1	3.1	0.016	0.019	0.025	0.031	0.037	0.043	0.050	—	—	—
	7	90	4.0	6.6	0.027	0.032	0.042	0.053	0.064	0.074	0.085	—	—	—
		180	6.6	6.6	0.033	0.040	0.053	0.066	0.079	0.092	0.106	—	—	—
	20	90	10.1	16.8	0.067	0.081	0.108	0.135	0.161	0.188	0.215	0.242	0.269	0.296
		180	16.8	16.8	0.084	0.101	0.134	0.168	0.202	0.235	0.269	0.302	0.336	0.370
Double vane (MSUB only)	1	90	1.1	1.1	—	0.007	0.009	0.011	0.013	0.015	0.018	—	—	—
	3	90	2.7	2.7	0.014	0.016	0.022	0.027	0.032	0.038	0.043	—	—	—
	7	90	5.7	5.7	0.029	0.034	0.046	0.057	0.068	0.080	0.091	—	—	—
	20	90	14.5	14.5	0.073	0.087	0.116	0.145	0.174	0.203	0.232	0.261	0.290	0.319

❻-1 Inner Volume and Air Consumption

Table (3) Rack & Pinion Style: Series CRJ

(L(ANR))

Size	Rotation (degree)	Volume VA (cm³)	Operating pressure (MPa)						
			0.15	0.2	0.3	0.4	0.5	0.6	0.7
05	90	0.15	0.00074	0.00089	0.0012	0.0015	0.0018	0.0021	0.0024
	180	0.31	0.0015	0.0018	0.0025	0.0031	0.0037	0.0043	0.0049
1	90	0.33	0.0016	0.0020	0.0026	0.0033	0.0039	0.0046	0.0052
	180	0.66	0.0033	0.0039	0.0052	0.0065	0.0078	0.0091	0.010

Table (4) Rack & Pinion Style: Series CRA1

(L(ANR))

Size	Rotation (degree)	Volume VA (cm³)	Operating pressure (MPa)									
			0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0
30	90	7.4	0.030	0.044	0.059	0.074	0.089	0.104	0.118	0.133	0.148	0.163
	180	14	0.056	0.084	0.112	0.140	0.168	0.196	0.224	0.252	0.280	0.308
50	90	32	0.128	0.192	0.256	0.320	0.384	0.448	0.512	0.576	0.640	0.704
	100	36	0.144	0.216	0.288	0.360	0.432	0.504	0.576	0.648	0.720	0.792
	180	65	0.260	0.390	0.520	0.650	0.780	0.910	1.040	1.170	1.300	1.430
	190	68	0.272	0.408	0.544	0.680	0.816	0.952	1.088	1.224	1.360	1.496
63	90	60	0.240	0.360	0.480	0.600	0.720	0.840	0.960	1.080	1.200	1.320
	100	67	0.268	0.402	0.536	0.670	0.804	0.938	1.072	1.206	1.340	1.474
	180	120	0.480	0.720	0.960	1.200	1.440	1.680	1.920	2.160	2.400	2.640
	190	127	0.508	0.762	1.016	1.270	1.524	1.778	2.032	2.286	2.540	2.794
80	90	111	0.444	0.666	0.888	1.110	1.332	1.554	1.776	1.998	2.220	2.442
	100	123	0.492	0.738	0.984	1.230	1.476	1.722	1.968	2.214	2.460	2.706
	180	221	0.884	1.326	1.768	2.210	2.652	3.094	3.536	3.978	4.420	4.862
	190	233	0.932	1.398	1.864	2.330	2.796	3.262	3.728	4.194	4.660	5.126
100	90	259	1.036	1.554	2.072	2.590	3.108	3.626	4.144	4.662	5.180	5.698
	100	288	1.152	1.728	2.304	2.880	3.456	4.032	4.608	5.184	5.760	6.336
	180	518	2.072	3.108	4.144	5.180	6.216	7.252	8.288	9.324	10.36	11.396
	190	547	2.188	3.282	4.376	5.470	6.564	7.658	8.752	9.846	10.940	12.034

Table (5) Rack & Pinion Style: Series CRQ2

(L(ANR))

Size	Rotation (degree)	Volume VA (cm³)	Operating pressure (MPa)										
			0.1	0.15	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0
10	90	1.2	—	0.006	0.007	0.009	0.012	0.014	0.016	0.018	—	—	—
	180	2.2	—	0.011	0.013	0.018	0.022	0.026	0.031	0.035	—	—	—
	360	4.3	—	0.021	0.026	0.034	0.043	0.051	0.060	0.068	—	—	—
15	90	2.9	—	0.015	0.017	0.023	0.029	0.035	0.041	0.046	—	—	—
	180	5.5	—	0.028	0.033	0.044	0.055	0.066	0.077	0.088	—	—	—
	360	10.7	—	0.023	0.064	0.086	0.107	0.129	0.193	0.172	—	—	—
20	90	7.1	0.028	0.036	0.043	0.057	0.071	0.085	0.099	0.114	0.128	0.142	0.156
	180	13.5	0.054	0.068	0.081	0.108	0.135	0.162	0.189	0.216	0.243	0.270	0.297
	360	26.3	0.105	0.131	0.158	0.210	0.263	0.316	0.368	0.421	0.473	0.526	0.578
30	90	12.1	0.048	0.060	0.073	0.097	0.121	0.145	0.169	0.193	0.218	0.242	0.266
	180	23.0	0.092	0.115	0.138	0.184	0.230	0.276	0.322	0.368	0.413	0.459	0.505
	360	44.7	0.179	0.224	0.268	0.358	0.447	0.537	0.626	0.716	0.805	0.895	0.984
40	90	20.6	0.082	0.103	0.123	0.164	0.206	0.247	0.288	0.329	0.370	0.411	0.452
	180	39.1	0.156	0.195	0.234	0.313	0.391	0.469	0.547	0.625	0.703	0.781	0.859
	360	76.1	0.304	0.380	0.456	0.609	0.761	0.913	1.07	1.22	1.37	1.52	1.67

Table (6) Rack & Pinion Style/Rotary Table: Series MSQ

(L(ANR))

Size	Rotation (degree)	Volume VA (cm³)	Operating pressure (MPa)									
			0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0
1	190°	0.66	0.0026	0.0039	0.0052	0.0065	0.0078	0.0091	0.010	—	—	—
2		1.3	0.0052	0.0077	0.010	0.013	0.015	0.018	0.021	—	—	—
3		2.2	0.0087	0.013	0.017	0.022	0.026	0.030	0.035	—	—	—
7		4.2	0.017	0.025	0.033	0.042	0.050	0.058	0.066	—	—	—
10		6.6	0.026	0.040	0.053	0.066	0.079	0.092	0.106	0.119	0.132	0.145
20		13.5	0.054	0.081	0.108	0.135	0.162	0.189	0.216	0.243	0.270	0.297
30		20.1	0.080	0.121	0.161	0.201	0.241	0.281	0.322	0.362	0.402	0.442
50		34.1	0.136	0.205	0.273	0.341	0.409	0.477	0.546	0.614	0.682	0.750
70		50.0	0.200	0.300	0.400	0.500	0.600	0.700	0.800	0.900	1.000	1.100
100		74.7	0.299	0.448	0.598	0.747	0.896	1.046	1.195	1.345	1.494	1.643
200		145.9	0.584	0.875	1.167	1.459	1.751	2.043	2.334	2.626	2.918	3.210

❻-2 Air Consumption Calculation Graph

Step 1 **Using Graph (16), air consumption volume of the rotary actuator is obtained. From the point of intersection between the internal volume and the operating pressure (slanted line) and then looking to the side (left side) direction, the air consumption volume for 1 cycle operation of a rotary actuator is obtained.**

Step 2 **Using Graph (17), air consumption volume of tubing or steel piping is obtainted.**
(1) First determine the point of intersection between the operating pressure (slanted line) and the piping length, and then go up the vertical line perpendicularly from there.
(2) From the point of intersection of an operating piping tube diameter (slanted line), then look to the side (left or right) to obtain the required air consumption volume for piping.

Step 3 **Total air consumption volume per minute is obtained as follows:**
(Air consumption volume of a rotary actuator [unit: L (ANR)] + Tubing or steel piping's air consumption volume) x Cycle times per minute x Number of rotary actuators = Total air consumption volume

Example) What is the air consumption volume for 10 units of a CRQ2BS40-90 to actuate by operating pressure 0.5 MPa for one minute..? (Distance between actuator and switching valve is the internal diameter 6 mm tubing with 2 m piping.)
1. Operating pressure 0.5 MPa → Internal volume of CRQ2BS40-90 40 cm^3 → Air consumption volume 0.23 L (ANR)
2. Operating pressure 0.5 MPa → Piping length 2 m → Internal diameter 6 mm → Air consumption volume 0.56 L (ANR)
3. Total air consumption volume = (0.23 + 0.56) x 5 x 10 = 39.5 L/min (ANR)

Inner Volume: Rack & Pinion Style

1 cycle (cm^3)

Model	Rotation angle				
	90°	100°	180°	190°	360°
CRJ □ 05	0.3	0.34	0.62	0.66	—
CRJ □ 1	0.66	0.74	1.32	1.4	—
CRA1□ 30	14.8	—	28	—	—
CRA1□ 50	64	72	130	136	—
CRA1□ 63	120	134	240	254	—
CRA1□ 80	222	246	442	466	—
CRA1□100	518	576	1040	1090	—
CRQ2□ 10	2.4	—	4.4	—	8.6
CRQ2□ 15	3.8	—	11	—	21.4
CRQ2□ 20	14.2	—	27	—	52.6
CRQ2□ 30	24.2	—	46	—	89.4
CRQ2□ 40	41.2	—	78.2	—	152
MSQ □ 1	—	—	—	1.3	—
MSQ □ 2	—	—	—	2.7	—
MSQ □ 3	—	—	—	4.4	—
MSQ □ 7	—	—	—	8.4	—
MSQ □ 10	—	—	—	13.1	—
MSQ □ 20	—	—	—	27.0	—
MSQ □ 30	—	—	—	40.2	—
MSQ □ 50	—	—	—	68.4	—
MSQB 70	—	—	—	100	—
MSQB 100	—	—	—	149	—
MSQB 200	—	—	—	292	—

Inner Volume: Vane Style

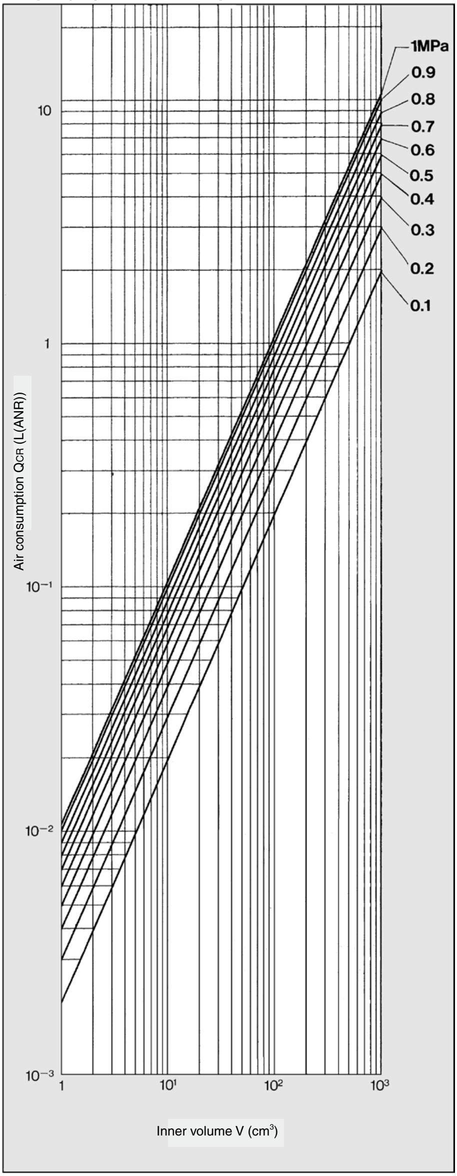
1 cycle (cm^3)

Model	Rotation angle					
	90°	100°	180°	190°	270°	280°
CRB □ 10-□S	1.6	—	2.4	—	3	—
CRB □ 15-□S	2.5	—	5.8	—	7.4	—
CRB □ 20-□S	8.4	—	12.2	—	15.8	—
CRB □ 30-□S	19.8	—	30	—	40	—
CRB □ 40-□S	25	—	31.5	—	41	—
CRB1□ 50-□S	60	64	98	102	132	136
CRB1□ 63-□S	70	73	94	97	118	121
CRB1□ 80-□S	176	186	276	286	376	386
CRB1□100-□S	372	394	562	584	752	774
MSU 1-□S	2.1	—	2.6	—	—	—
MSU 3-□S	5.0	—	6.2	—	—	—
MSU 7-□S	10.6	—	13.2	—	—	—
MSU 20-□S	26.9	—	33.6	—	—	—
CRB 10-□D	2	2.2	—	—	—	—
CRB 15-□D	5.2	5.4	—	—	—	—
CRB 20-□D	11.2	11.4	—	—	—	—
CRB 30-□D	28.8	29	—	—	—	—
CRB 40-□D	33	34	—	—	—	—
CRB1□ 50-□D	96	104	—	—	—	—
CRB1□ 63-□D	98	104	—	—	—	—
CRB1□ 80-□D	272	292	—	—	—	—
CRB1□100-□D	544	588	—	—	—	—
MSUB 1-□D	2.2	—	—	—	—	—
MSUB 3-□D	5.4	—	—	—	—	—
MSUB 7-□D	11.4	—	—	—	—	—
MSUB 20-□D	29.0	—	—	—	—	—

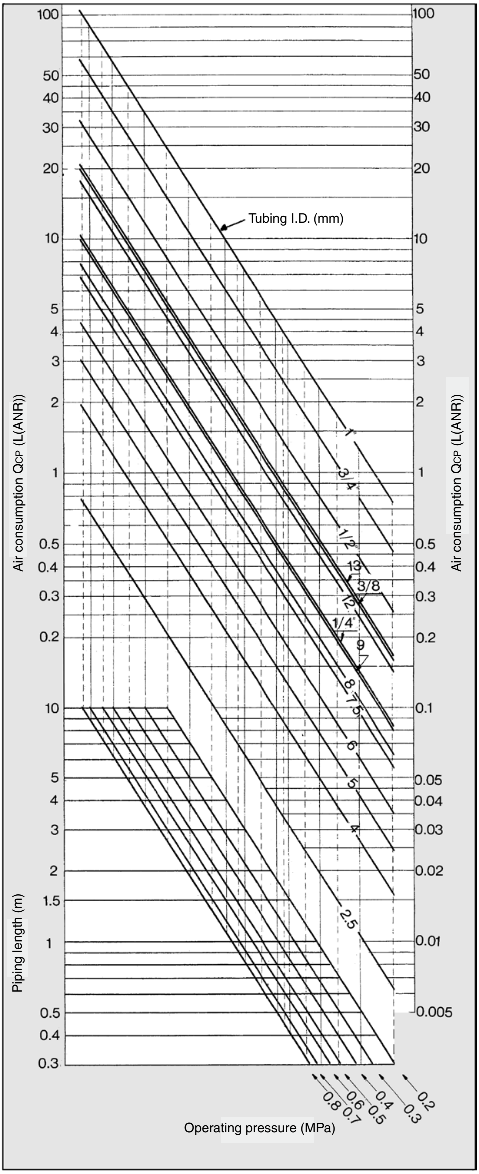
Rotary Actuators Model Selection

❻-2 Air Consumption Calculation Graph

Graph (16) Air Consumption



Graph (17) Air Consumption of Tubing, Steel Tube (1 cycle)



∗ “Piping length” indicates length of steel tube or tubing which connects rotary actuator and switching valves (solenoid valves, etc.).

∗ Refer to page 40 for size of steel tubing (inner dimension and outer dimension).